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(54) Sparger for direct oxygen injection into a reactant stream for a fluidized bed reactor

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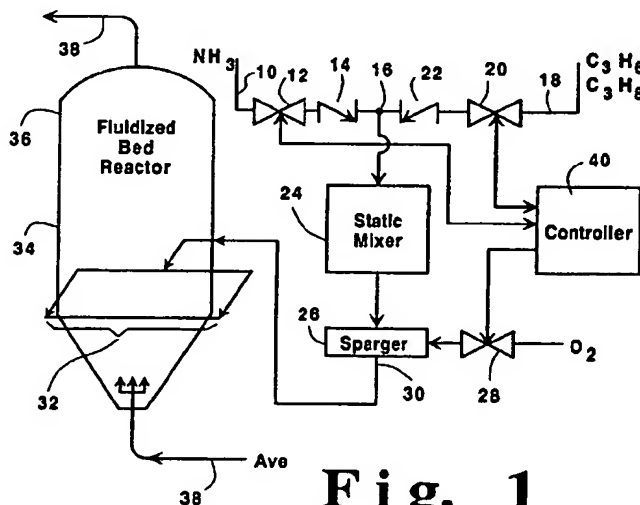


Fig. 1

EP 0 761 298 A2

Description

Field of the Invention

This invention relates to a sparger for entraining an oxygen-bearing gas into a reactant stream which is fed to a fluidized bed reactor and, more particularly, to a sparger for injection of oxygen into a reactant feed stream to a fluidized bed reactor that is employed in an acrylonitrile synthesis process.

Background of the Invention

The production of nitriles involves ammoxidation of an appropriate alkene in the presence of a suitable catalyst. Acrylonitrile production employs feeds of propylene and ammonia into an ammoxidation reactor where, in the presence of air/oxygen and a suitable catalyst, acrylonitrile is produced with lesser amounts of other nitrogen-containing compounds and carbon oxides. The reactor is often a fluidized bed reactor which includes a separate air injection conduit for introduction of either air or enriched air (with added oxygen) into the fluidized bed. Effluent from the ammoxidation reaction is quenched with water, as desired products are obtained in the liquid phase.

To provide oxygen for the conversion of the mixture of propylene and ammonia to acrylonitrile, the prior art has suggested the addition of oxygen or oxygen-containing gas directly to the feed flow or as a separate feed to the reactor. Such teachings can be found in U.S. Patent 4,609,502 to Khoobiar et al. and U.S. Patent 4,868,330 of Ramachandran et al. Neither of the afore-said patents provides any teaching that an oxygen deficiency can occur in a fluidized bed reactor at the point of reactant feed introduction. Ramachandran et al. teach that when a pure oxygen feed is present in the ammoxidation reactor, that a gaseous flame suppressor mixture be utilized, e.g., carbon dioxide in an amount of about 25-70% by volume. As a result, Ramachandran et al. provides further apparatus downstream from the ammoxidation reactor to recover and recycle the carbon dioxide.

Other references which teach further details regarding acrylonitrile production are: U.S. Patent 4,754,049 to Khoobiar et al.; and U.S. Patents 4,849,537, 4,849,538, 4,870,201 and 5,015,756, all to Ramachandran et al. While, as above indicated, the prior art teaches the addition of oxygen or oxygen-bearing gases into a feed stream to an ammoxidation reactor, none of the cited patents provide details as to equipment for such gaseous addition/mixing.

U.S. Patent 3,661,165 to Rainbird et al. discloses a sparger valve for the mixing of oxygen with gaseous hydrocarbons in a process stream. The Rainbird et al. sparger valve includes a number of jets facing downstream within the hydrocarbon gas flow. The jets introduce oxygen at a jet velocity that is substantially higher than the velocity of the hydrocarbon gas. Variations in

oxygen mass flow are achieved by varying the area of the jet orifices, while maintaining a predetermined pressure drop across the orifices.

U.S. Patent 5,356,213 to Arpentinier describes a further sparger design which is positioned coaxially with respect to the axis of a channel containing a feed stream. Radial vanes are employed in the sparger to enable injection of gas in a substantially radial direction towards the outside of the feed flow so as to enable a mixing of the injected gas with the feed flow gas.

The above noted prior art includes no teaching of fluidized bed reactor performance penalties which occur as a result of oxygen deficiencies at points of feed stream introduction. Further, the prior art, while including teachings regarding the introduction of oxygen-bearing gases at various points in a process, includes no teachings of how such an introduction can be accomplished in a manner to assure process safety.

Accordingly, it is an object of this invention to provide an improved sparger for enabling an oxygen bearing gas to be combined with a gaseous reactant feed flow to a fluidized bed reactor.

It is another object of this invention to provide an improved sparger for combining an oxygen-bearing gas and gaseous reactants in a manner to avoid explosions, deflagration or other anomalous effects in the process.

SUMMARY OF THE INVENTION

A system provides an oxygen-bearing gas and gaseous reactants to a fluidized bed reactor. Oxygen is introduced into the reactant gas stream by a sparger of a preferred design. A preferred embodiment of the sparger is a circular or closed polygonal annulus with downstream-pointing orifices which issue an oxygen bearing gas into the mixed reactant gas stream. The sparger's orifices are sufficiently separated to prevent a mixing from adjacent orifices of flammable combinations of the oxygen bearing gas and the reactant gas stream. Inner and outer diameters of the sparger annulus are set to assure that approximately equal quantities of the reactant gas stream pass both inside and outside the sparger annulus. Other sparger arrangements are also described.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a block diagram of a system that embodies the invention hereof.

Fig. 2 is a sectional view of a feed pipe which includes a preferred embodiment sparger design for introducing oxygen into a gaseous feed stream.

Fig. 3 is a schematic view of a pair of adjacent jets of the sparger of Fig. 2.

Fig. 4 is a schematic view of a feed pipe which includes a second sparger configuration with plural annuli for introducing oxygen into a gaseous feed stream.

Fig. 5 is a schematic view of a feed pipe which

includes a third sparger configuration for introducing oxygen into a gaseous feed stream.

Fig. 6 is a schematic view of a feed pipe which includes a fourth sparger configuration for introducing oxygen into a gaseous feed stream.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

Turning to Fig. 1, a system is shown for producing acrylonitrile using a fluidized bed ammoxidation process. A conduit 10 provides a flow of ammonia through a control valve 12, a check valve 14 to a T-junction 16. In similar fashion, a flow of propylene and propane are fed via conduit 18 through a control valve 20, check valve 22 to T-junction 16. There, the combined feed gases are fed to a static mixer 24 where they are combined into a mixed gaseous reactant stream that is, in turn, fed to a sparger 26. An oxygen source is connected via a control valve 28 to sparger 26.

Sparger 26 thereby enables oxygen to be entrained into the mixed reactant gas stream and to pass via conduit 30 to feedlines 32. Feedlines 32 are in direct contact with a fluidized bed 34 which comprises a particulate catalyst that facilitates a reaction occurring between the ammonia, propylene and oxygen constituents to produce an acrylonitrile product. That product is output from reactor 36 via conduit 38 where it is subjected to further processing. At the bottom of reactor 36 is an air feed 38 which provides additional oxygen for the reaction.

A controller 40 includes control connections to each of valves 12, 20 and 28 and serves to control reactant feeds therethrough in accordance with sensed process conditions. The process inputs to controller 40 are not shown in the figure. Those skilled in the art will realize that a single controller 40 is shown only for explanatory purposes and that plural controllers can be used to control the various valves and other control entities. Controller 40, under user operation, assures that sufficient oxygen is injected by sparger 26 into the feed stream to assure, at the points of injection within fluidized bed reactor 36, that sufficient oxygen is present to prevent an oxygen deficiency at such points of injection. Controller further assures that the mixed concentration of reactants and oxygen is kept above an upper flammability limit (UFL) of the mixture. An acceptable safety margin of at least 25%, and preferably 50%, should be maintained.

The direct injection of oxygen with the reactants enables a concentration of oxygen at the region of feed injection which enables both a yield improvement and catalyst lifetime extension. Air flow into reactor 36, via conduit 38 also is adjusted to assure that the proper amount of oxygen is entrained within the reactor fluidized bed to enable optimum reaction conditions to be achieved. It is vital to the invention that plural oxygen supplies be provided to fluidized bed reactor 36, one supply assuring a proper oxygen concentration at the

immediate regions of feed injection and the second oxygen supply assuring overall appropriate oxygen availability within the fluidized bed to enable proper reaction conditions to be achieved.

As indicated above, the feed flow of oxygen through sparger 26 is maintained at a level to assure that the upper flammability limit of the mixed reactant gas stream is exceeded. Table 1 below shows both the upper and lower flammability limits (UFL and LFL) for a propylene/ammonia feed stream in 100% oxygen.

TABLE 1

Calculated Flammability Limits in 100% oxygen		
	LFL	UFL
Propylene Feed ^a	2.3	53.5
Ammonia Feed ^b	14.6	79.7
Combined Feed ^c	4.1	64.6

a. 94% propylene, 6% propane, 150°F, 30 psig

b. 100% ammonia, 1500F, 30 psig

c. 52.4% ammonia, 44.7% propylene, 2.9% propane, 150°F, 30 psig

Sparger 26 is shaped to allow its injectors to be arranged in pattern that achieves effective oxygen distribution throughout the reactant gas flow. The injectors are further positioned so as to prevent interaction of flammable mixtures which occur within the feed stream. In Fig. 2, sparger 26 is positioned within conduit 30 and is preferably shaped in the form of a single ring 50 that is positioned normal to the feed gas flow. Ring 50 may be either a continuous circle or a closed multi-sided polygon. To achieve good gas distribution, the inner and outer diameters of ring 50 are set so that there is substantially equal gas flow in regions 52 and 54, respectively. Thus, the effective cross-sectional areas of regions 52 and 54 are made approximately equal by appropriate sizing of ring 50. This arrangement assures that a low pressure area is not formed in the feed pipe within the ring of orifices (injectors) which would draw together the jets and create a severe problem in the event of an ignition of one of the jets.

Within ring 50 is a channel 56 which communicates with valve 28 (see Fig. 1) via inlet 58. A plurality of fixed jets 60 are positioned about ring 50 and are oriented so as to direct oxygen outflow from channel 56 in a downstream direction within conduit 30.

A sectional view of a pair of jets 60' and 60" is shown in Fig. 3. Oxygen flows out of jets 60' and 60" and creates substantially pure oxygen regions 70 and 72. The mixed reactant feed gas is present in regions

74, 74' and 74". Within regions 76 and 78 (cross-hatched), a mixture of oxygen and reactants occurs which is within the flammable ranges. Further downstream (regions 80 and 82), the gaseous mixture is non-flammable, even though oxygen bearing.

The spacing D between adjacent jets 60' and 60" is adjusted so that the flammable regions 76 and 78 do not interact. The limitation of jet-to-jet interaction reduces the probability of a once ignited jet causing ignition of another jet and of the jets coalescing to form a single jet with a large flame volume. The orifices of adjacent jets are thus placed so that neighboring regions of flammable gas mixture do not interact. Further, the mixed gas regions from adjacent jets intersect at a point beyond the farthest extent of the flammable regions. The risk of ignition is further reduced by lowering the total combined flammable volume contained within each oxygen jet. This is accomplished by minimizing the orifice diameter of each jet which, in turn, tends to maximize the number of orifices to accomplish a desired oxygen flow level.

The distance between a center of one orifice to the center of an adjacent orifice is given by:

$$D \geq d_o \{(258.7 - \text{UFL}) / (100 - \text{UFL})\}$$

where:

D = center - center distance between orifices;

d_o = orifice diameter;

UFL = upper flammability limit (in percent).

A risk of sustained jet deflagration is further reduced by insuring that the oxygen jet velocity is appreciably greater than both the velocity of the gaseous feed reactants and the flame velocity of a flammable oxygen-reactant mixture. Such a jet velocity promotes flame blowoff, should flaming occur. To encourage blowoff, the initial oxygen jet velocity is preferably at least twice either the feed velocity of the reactant stream or flame velocity, whichever is greater. Further, the sparger is not to be constructed out of square shaped tubing or to be supported by angle iron. Such structures include sharp angles which create eddies that can enhance flame stability.

Returning to Fig. 1, controller 40 operates valves 12, 20 and 28 to provide about one part ammonia, one part propylene and ten parts of air to fluidized bed reactor 36. The injection of oxygen, via valve 28 and sparger 26, enables a modest reduction in air flow via conduit 28. In addition to assuring that the combined reactant/oxygen flow in conduit 30 is in excess of the upper flammability level, it is preferred that the volumetric outflow from sparger 26 does not exceed a relative volumetric flow as follows: oxygen 30%; ammonia 35%; and propylene 35%. More preferably, the volumetric ratios are as follows: 10% oxygen; 45% ammonia; and 45% propylene.

If oxygen flow is suddenly increased or the reactant

feed flow suddenly decreased, it is possible that the output from sparger 26 may move into a detonatable region. To control a sudden increase in oxygen flow, valve 28 is provided with a critical flow orifice which limits the possible oxygen flow. The orifice is sized so that even if valve 28 fails in the full-open state, the amount of oxygen required to produce a detonation under normal minimum feed flow rates cannot be supplied.

During emergency process shutdown, so long as the oxygen flow to sparger 26 is shut down simultaneously with the process reactants, the oxygen flow will be stopped simultaneously with the stoppage of reactant flow. Since oxygen valve 28 is significantly smaller than either of feed valves 12 and 20, the oxygen flow will stop before the flow of reactants - thereby preventing a feed concentration build-up to a detonatable level.

Controller 40 is operated to shut the oxygen flow to sparger 26 if the feed reactant pressures drop below a certain level. This is because a significant drop in feed-flow can be brought about by feed blockage and a pressure-based shut-down response of valve 28 prevents a possible subsequent detonatable mixture from entering conduit 30.

Additionally, controller 40 is operated to shut the oxygen flow to sparger 26 if the temperature of the mixed oxygen reactant stream goes above a certain level. This is because a significant increase in gas mixture temperature can be brought about by a deflagration near the sparger and a temperature-based shut-down response of valve 28 will extinguish such a deflagration.

Valve 28 is also controlled by controller 40 to assure certain minimum oxygen flows to sparger 26. In operation, reactant feed must be prevented from backstreaming into sparger 26. This is prevented by: maintaining an oxygen flow through each sparger jet 60; maintaining a jet velocity that is great enough to prevent a convective or diffusive flow of the reactant feed into sparger 26; and placing the jets on the downstream side of sparger 26. The maintenance of oxygen flow through each sparger jet 60 is accomplished by insuring that the pressure drop across the jets 60 is significantly greater than the pressure drop within sparger 26. To prevent the reactant feed from diffusing into sparger 26, it is preferred that a minimum pressure drop across each jet 60 be at least 1 psi and preferably 10 psi.

Finally, during startup, a nitrogen purge is used to flush sparger 26 of reactants before oxygen flow begins. During shutdown, sparger 26 is flushed of oxygen with a nitrogen purge while maintaining a high enough pressure drop to prevent backstreaming. This is necessary because reactants will flow into sparger 26 after shutdown.

While sparger 26 has been shown in the shape of a ring, other shapes such as concentric rings (see Fig. 4), straight tubing (see Fig 5) and crossed tubing (see Fig. 6) are acceptable. However, each such structure must meet the requirements set forth above with respect to the most preferred embodiment, i.e., the circular sparger configuration shown in Fig. 2. Importantly, the

distance between adjacent orifices must be as described above. Further, rather than placing the jets directly on the downstream edge of sparger 26, they can be placed off center, but still on the downstream side. This may be beneficial as it allows for a greater number of jets to be employed.

While the above description has focused on use of the invention in an acrylonitrile production process, other gas phase oxidations that use fluidized beds may also employ the invention (e.g., processes for the production of maleic anhydride, phthalic anhydride synthesis, etc.). While not as preferred, inert gases may be added to either the oxygen or the reactant feed streams to lower the upper fire limit and thus increase the maximum concentration of oxygen allowed in the feed stream.

It should be understood that the foregoing description is only illustrative of the invention. Various alternatives and modifications can be devised by those skilled in the art without departing from the invention. Accordingly, the present invention is intended to embrace all such alternatives, modifications and variances which fall within the scope of the appended claims.

Claims

1. A sparger for providing a mixture of an oxygen-bearing gas and a gaseous reactant stream, comprising:

a pipe for providing said gaseous reactant stream in a downstream direction;

at least one annular conduit positioned within said pipe, transverse to gas flow in said pipe, and connected to a source of oxygen-bearing gas, said annular conduit provided with orifices thereabout that point generally in said downstream direction, for injecting said oxygen-bearing gas into said gaseous reactant stream.

2. The sparger as recited in claim 1, wherein said annular conduit is circular and provides a continuous interior flow path for said oxygen-bearing gas.
3. The sparger as recited in claim 1, wherein said annular conduit is a closed multi-sided polygonal annulus and provides a continuous interior flow path for said oxygen-bearing gas.
4. The sparger as recited in claim 1, wherein an outer circumference and an inner circumference of said annular conduit are sized so that approximately equal volumes of said reactant gas stream flows between said outer circumference and an inner surface of said pipe, and within said inner circumference of said annular conduit.
5. The sparger as recited in claim 1, wherein said ori-

fices are positioned sufficiently far apart on said annular conduit to prevent flammable mixtures of said reactant gases and said oxygen-bearing gas from interacting downstream from adjacent orifices.

6. The sparger as recited in claim 1, wherein said orifices are of fixed size, said oxygen-bearing gas is oxygen, and said sparger is installed in a system which comprises:

means for pressurizing said source of oxygen to assure that no reactant gases flow into said sparger during operation thereof.

7. The sparger as recited in claim 6, wherein said system further comprises:

control means coupled to plural sources of gaseous reactants and a source of oxygen, for adjusting feeds of said gaseous reactants in said pipe and oxygen to said annular conduit to assure that said reactant gas stream and oxygen is maintained above an upper flammability limit downstream from said sparger.

8. A sparger for providing a mixture of an oxygen-bearing gas and a gaseous reactant, comprising:

a pipe for providing a reactant gas stream in a downstream direction;
at least one conduit positioned within said pipe, transverse to gas flow in said pipe, and connected to a source of oxygen-bearing gas, said conduit provided with orifices thereabout that point generally in said downstream direction, for injecting said oxygen-bearing gas into said reactant gas stream, said orifices positioned sufficiently far apart on said conduit to prevent flammable mixtures of said reactant gases and said oxygen-bearing gas from interacting downstream from adjacent orifices.

9. The sparger as recited in claim 8, wherein said orifices are of fixed size, said oxygen-bearing gas is oxygen, and said sparger is installed in a system which comprises:

means for pressurizing said source of oxygen to assure that no reactant gases flow into said sparger during operation thereof.

10. The sparger as recited in claim 9, wherein said system further comprises:

control means coupled to plural sources of gaseous reactants and a source of oxygen, for adjusting feeds of said gaseous reactants in said pipe and oxygen to said conduit to assure that said reactant gas stream and oxygen is

maintained above an upper flammability limit
downstream from said sparger.

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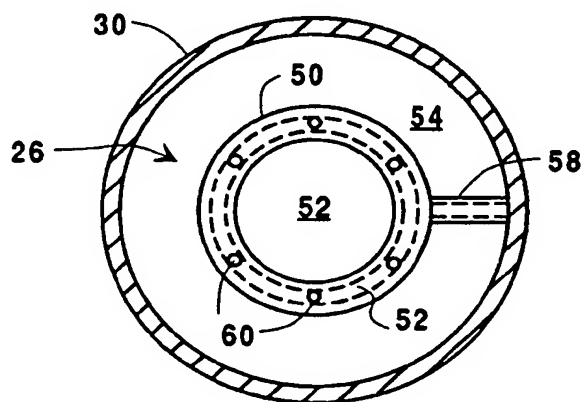
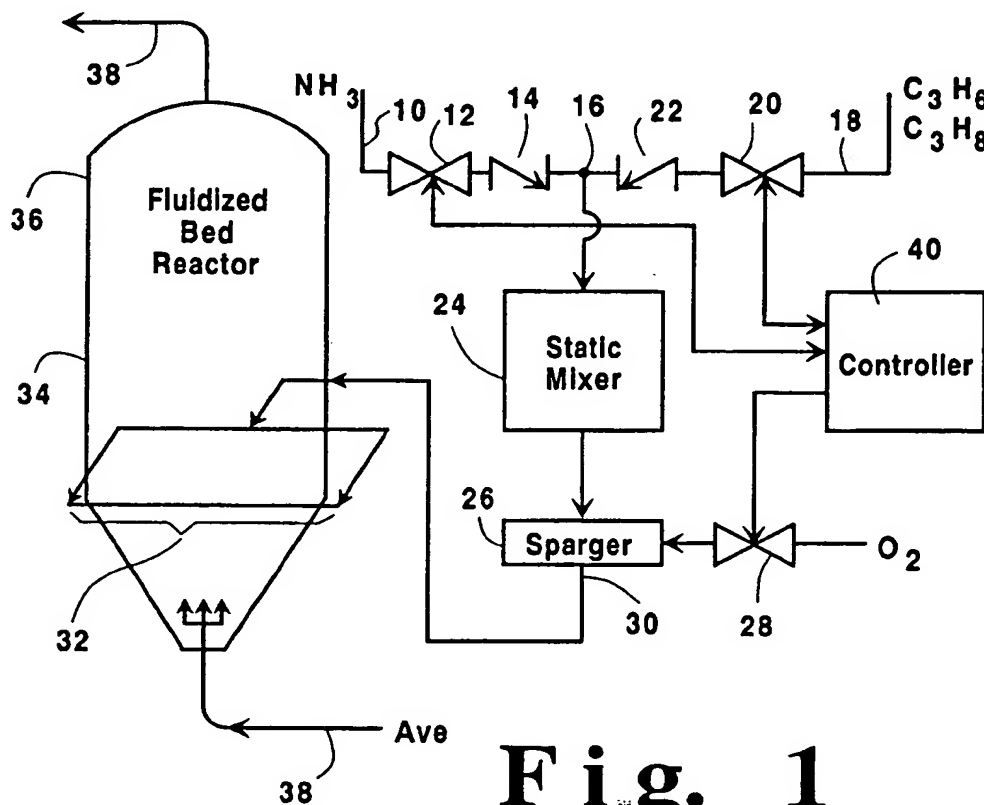
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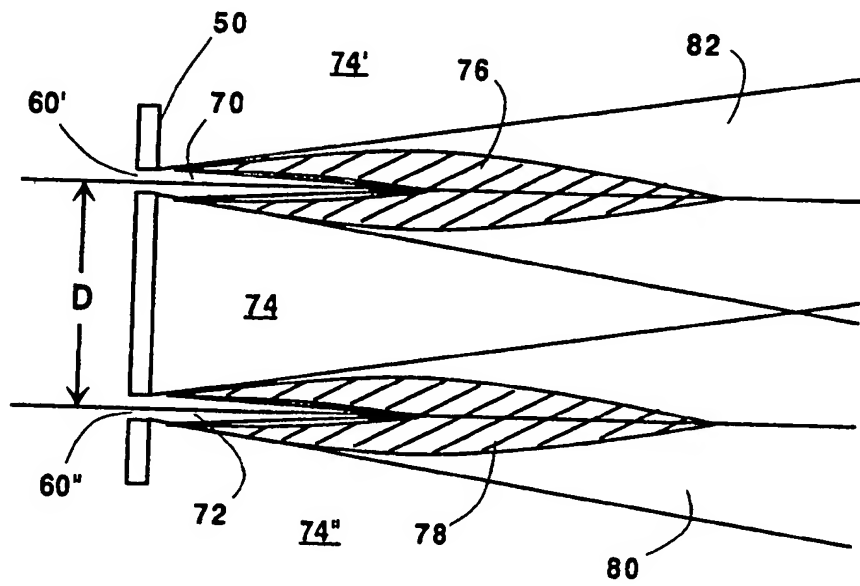


Fig. 3

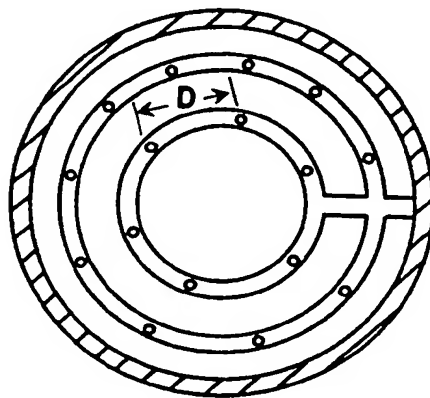


Fig. 4

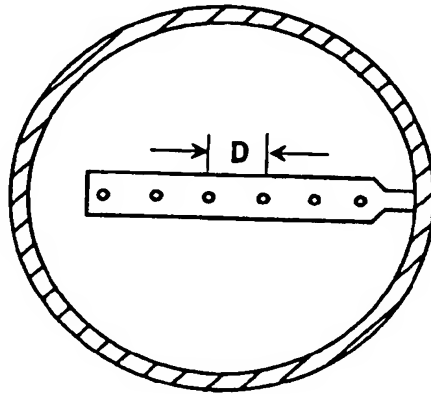


Fig. 5

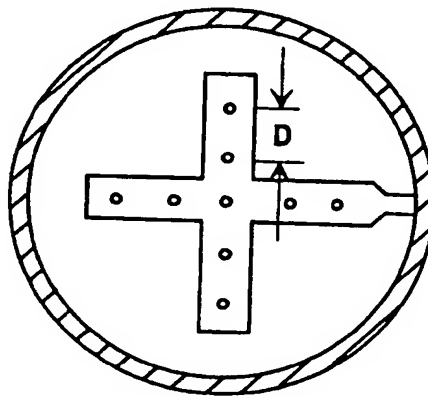


Fig. 6

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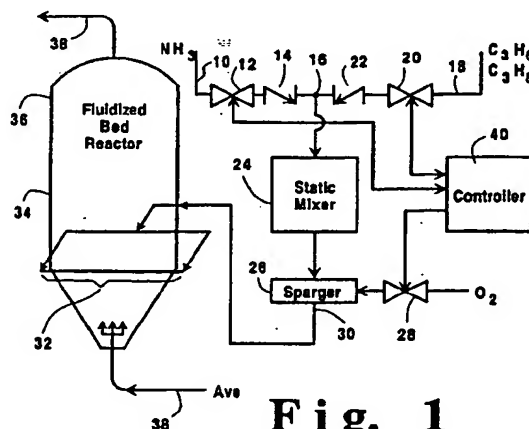
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EUROPEAN SEARCH REPORT

Application Number
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DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	US 3 702 619 A (SHELL OIL COMPAGNY) 14 November 1972 * column 1, line 16 - line 17; claims 1,2; figures 1,2 * * column 1, line 26 - line 32 * * column 1, line 35 - line 48 * * column 2, line 23 - line 33 * * column 3, line 58 - line 59 * * column 4, line 9 - line 13 * * column 6, line 20 - line 29 * * column 6, line 37 - line 42 * * column 6, line 54 - line 59 * * column 7, line 30 - line 41 *	1,2,6,7	B01J8/24 B01J19/00 B01F5/04 B01J4/00 B01J8/18
A	-----	5,8-10	
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			B01J B01F
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 8 April 1997	Examiner Lapeyrere, J
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